

## Fine Structure Calculations of the Energy Levels, Oscillator Strength and Transition Probabilities for As Like Gallium

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### Abstract

Fine structure calculations of the energy levels, the wavelengths, the oscillator strengths, log gf and the transition probabilities for transitions among the terms belonging to  $1s^2 2s^2 2p^6 3s^2 3p^6 3d^{10}ns$ ,  $n=5-10$ ,  $1s^2 2s^2 2p^6 3s^2 3p^6 3d^{10}np$ ,  $n=4-10$ ,  $1s^2 2s^2 2p^6 3s^2 3p^6 3d^{10}nd$ ,  $n=4-10$  and  $1s^2 2s^2 2p^6 3s^2 3p^6 3d^{10}nf$ ,  $n=4-10$  configurations of As (III) have been calculated using configurations interaction Cowan atomic structure code. Our calculated values for the above mentioned quantities have been compared with the corresponding experimental data and other theoretical calculations where a satisfactory agreement has been obtained. We also report on some unpublished corresponding values for As like gallium.

### 1. Introduction

Spectroscopic data of gallium [1, 2] and gallium-like ions [3-5] may be of interest for plasma investigations in controlled thermonuclear fusion experiments. Recently, multicharged ion spectra of the gallium isoelectronic sequence ( $Z>35$ ) have been analyzed. In particular, spectra of the Rb VII ion emitted from sparks and laser-produced plasmas have been investigated [6]. At the same time there are an extensive experimental and theoretical spectroscopic studies for the Gallium like ions. The first six elements of the gallium sequence have been calculated using the multiconfiguration optimised potential model [7].

Gallium isoelectronic sequence has been studied for some transitions using the configuration interaction approach [8]. Multiconfiguration Dirac-Fock calculations on multi-valence-electron systems have been also performed for Ga-like ions [9]. In addition, spectra of the gallium-like ions excited by low-inductance sparks and laser-produced plasmas were observed [10]. Oscillator strengths for excitations of As I-III are calculated using a semiempirical analytic independent-particle-model [11]. Also the energy levels and observed spectral lines of Krypton, Kr I through Kr XXXVI have been studied [12].

The configuration interaction (CI) approach has been used to account for electron correlation effects. To visualize these effects we also include some single configuration results. Two self-consistent-field methods are used to generate orbitals required to construct a multiconfiguration wavefunction. One of them is the Hartree-Fock method with taking into account the relativistic corrections (HFR) and the other one is also Hartree Fock method

but without considering the relativistic corrections.

It is found that COWAN code in addition to parametric fit approach is a useful tool for heavy manyelectron systems where intravelence electron correlation plays an essential role. The purpose of this paper is to report new calculations involving higher energy levels, wavelengths, oscillator strengths and transition probabilities that are not calculated before beside the precalculated data to indicate the reliabilities of the new ones by making comparisons with the available theoretical and experimental data.

In the present work, energy levels, wavelengths, log gf, oscillator strengths, and transition probabilities have been calculated for transitions among the terms belonging to  $1s^2 2s^2 2p^6 3s^2 3p^6 3d^{10}ns$ ,  $n=5-10$ ,  $1s^2 2s^2 2p^6 3s^2 3p^6 3d^{10}np$ ,  $n=4-10$ ,  $1s^2 2s^2 2p^6 3s^2 3p^6 3d^{10}nd$ ,  $n=4-10$  and  $1s^2 2s^2 2p^6 3s^2 3p^6 3d^{10}nf$ ,  $n=4-10$  configurations of As like gallium [13].

### 2. Method of calculations

Theoretical treatment of an atom containing N electrons requires first of all a knowledge of a suitable Hamiltonian operator. An operator over all N electrons, and adding a term for electrostatic coulomb interactions among electrons [14]

$$\begin{aligned} H &= H_{\text{kin}} + H_{\text{elec-nucl}} + H_{\text{elec-elec}} + H_{\text{S-O}} \\ &= \sum_{i=1}^n \nabla_i^2 - \sum_{i=1}^N \frac{2Z}{r_i} + \sum_{i>j}^N \sum_{i=1}^N \frac{2}{r_{ij}} + \sum_{i=1}^N \xi_i(r_i)(l_i - s_i) \end{aligned} \quad (1)$$

where  $r_i = |\mathbf{r}_i|$  is the distance of the  $i^{\text{th}}$  electron from the nucleus,  $r_{ij} = |\mathbf{r}_i - \mathbf{r}_j|$  is

the distance between the  $i^{\text{th}}$  and  $j^{\text{th}}$  electron, and  $\xi(r_i)$  is a radial proportional factor. It should be noticed that in a multi-electron atom, other magnetic interactions may be considered such as: orbital-orbital, spin-spin, and spin-other orbit interactions. But these interactions are usually much less important than the spin-orbital interaction, thus they can be neglected. Each electron in a many electron atom is considered to move in a central potential independently of the others [15], at least in the first approximation. The  $i^{\text{th}}$  electron may then be described by the function  $\Psi_{\alpha}(i)$  which is given in terms of a product of radial, spherical harmonic and spin wave functions :-

$$\Psi_{\alpha}(i) = \Psi_{n\ell m_{\ell} m_s}(i) = R_{n\ell}(r_i) Y_{\ell}^{m_{\ell}}(\theta_i, \phi_i) \chi_{m_s}(i) \tag{2}$$

where  $R_{n\ell}(r_i)$  is the radial function,  $Y_{\ell}^{m_{\ell}}(\theta_i, \phi_i)$  is the spherical harmonic function,  $\chi_{m_s}(i)$  is the spin function,  $n$  is the principal quantum number,  $m_{\ell}$  is the z-component of the electron orbital angular momentum quantum number, and  $m_s$  is the z-component of the electron spin quantum number.

For N-electrons, the Pauli principle requires that each set of quantum numbers:  $\alpha, \beta, \gamma, \dots, \nu$  should be different from one electron to other. This means that a simple N-electron wave function will consist of a direct product of single-electron wave functions:

$\Psi_{\alpha}(1)\Psi_{\beta}(2)\Psi_{\gamma}(3)\dots\Psi_{\nu}(N)$  The Pauli principle can be included in a more general symmetry principle, produced by Heisenberg and Dirac. Slater showed that this requirement could be satisfied by a normalized determinantal product wave function of the form:-

$$\Psi(\alpha, \beta, \dots, \nu) = \frac{1}{\sqrt{N!}} \begin{vmatrix} \Psi_{\alpha}(1) & \Psi_{\alpha}(2) & \dots & \Psi_{\alpha}(N) \\ \Psi_{\beta}(1) & \Psi_{\beta}(2) & & \Psi_{\beta}(N) \\ \dots & & & \\ \Psi_{\nu}(1) & \Psi_{\nu}(2) & \dots & \Psi_{\nu}(N) \end{vmatrix} \tag{3}$$

In practice the linear combinations of such determinant functions for single configurations are formed which are angular eigenstates in an appropriate coupling scheme and these form the basis states for the multi-configuration expansions.

The matrix elements of the Hamiltonian between determinant functions can be reduced to one and two electron terms so that for states B and B' [13]:

$$\langle B|H|B' \rangle = E_{av} \delta_{BB'} + \sum_{ijk} [f_k F^k(\ell_i, \ell_j) + g_k G^k(\ell_i, \ell_j)] + \sum_i d_i \zeta(\ell_i) \tag{4}$$

where  $E_{av}$  is the central field energy. Furthermore, modest ad hoc scaling adjustments are applied to the F, G, and d to allow for configurations omitted from the multi-configuration expansion. The wave functions obtained from equation (3) are used to calculate the excitation energies of the fine structure levels, the oscillator strengths and the transition probabilities. The calculations are carried out in intermediate coupling scheme. A choice of nomenclatures is possible in seeking to assign angular quantum numbers as identifiers of the intermediate coupling numerical eigen states. Since only parity and total angular momentum observables commute with the Hamiltonian, other quantum number assignments are approximated one. In these assignments we are led by angular momentum coupling schemes appropriate to the dominant parts of the Hamiltonian. One of them is known as the LS-scheme when the electrostatic terms dominate and the other is known as the jj-scheme when relativistic terms dominate. The code identifies the energy eigen states by dominant component in its expansion in a particular basis.

The radial function is obtained as the solution of the following equation [13,16]:

$$\left[ \frac{d^2}{dr^2} + \frac{\ell_i(\ell_i + 1)}{r^2} + V_i(r) \right] R_{n\ell}(r) = \varepsilon_i R_{n\ell}(r)$$

The solution of the above Shrodinger equation (the radial wave function  $R_{n\ell}$ ) is analogous to the behavior of legendre  $P_{n\ell}$  for which we have

$$\int_0^{\infty} P_{n\ell}(r) P_{n'\ell}(r) dr = \delta_{nn'} ; \quad \ell + 1 < n \leq n$$

where  $V_i$  is the central potential seen by the  $i^{\text{th}}$  electron and  $\varepsilon_i$  is the single particle energy. An optimised potential is obtained variationally. It is noticeable that the present code uses the Relativistic Hartree Fock method of Cowan [13].

### 2.1 Spontaneous transitions between degenerate levels

The radiative decay rate between degenerate levels p and q is given by [17]:

$$A_{pq} = \frac{e^2 W_{pq}^3}{3\pi \varepsilon_0 \hbar c^3} \sum_{m_q} | \langle q m_q | r | p m_p \rangle |^2$$

(5) where  $m_p$  and  $m_q$  are the magnetic orbital quantum numbers of the involved levels,  $e$  is the electron charge,  $c$  is the speed of light,  $W$  is the angular frequency of the transition photon, and  $\varepsilon_0$  is the vacuum permittivity.

The decay rate can be made more symmetrical by introducing an additional summation over mp and dividing by the statistical weight  $g_p=2j_p+1$  of the upper level:

$$A_{pq} = \frac{e^2 w_{pq}^3}{3\pi\epsilon_0 \hbar c^3} \frac{1}{g_p} \sum_{m_p m_q} |\langle qm_q | r | pm_p \rangle|^2 \quad (6)$$

The radiative life time  $\tau_p$  of an excited atomic state p is related to the atomic transition probability  $A_{pq}$  by:

$$\tau_p = 1 / \sum A_{pq} \quad (7)$$

where, the sum is extended over all the lower states which can be reached from the upper state by radiative decay.

## 2.2 Oscillator strengths:

The oscillator strength or f-value describes what fraction of the energy of the classical oscillator should be ascribed to a given transition [17]. For transitions from an upper level p to a lower level q, the emission f-value,  $f_{pq}$  is given by the following relation.

$$A_{pq} = -3fpq \gamma \quad (8)$$

where:

$$\gamma = \frac{e^2 w^3}{6\pi\epsilon_0 m c^3}$$

is defined as the classical transition probability. While for an upward transition from level q to level p, the absorption f-value,  $f_{qp}$ , is defined by:

$$g_q f_{qp} = -g_p f_{pq} \quad (9)$$

The explicit expressions for the transition probability  $A_{pq}$  in terms of the emission and the absorption oscillator strengths are given now by the following relation:

$$A_{pq} = \frac{e^2 w_{pq}^3}{2\pi\epsilon_0 m c^3} (-f_{pq}) = \frac{e^2 w_{qp}^3}{2\pi\epsilon_0 m c^3} \left(\frac{g_q}{g_p} f_{qp}\right) \quad (10)$$

## 3. Results and discussion

### 3.1 Energy levels

In general, with one electron outside a closed shell, correlation in the core is negligible [14]. The energy of the electronic configurations are obtained by adjusting the scaling parameters  $E_{av}$  and  $\zeta_i(r_i)$  that are shown in tables 1. The energy levels for As like gallium have been tabulated in tables 2. Our calculations of energy levels have been compared with data relative to NIST From the comparison we found that all the calculated energy levels are almost the same to the value of NIST [18].

### 3.2 Wavelengths, oscillator strengths and transition probabilities

In tables 3 we have tabulated our calculated wavelengths,  $\lambda$  (Å), the absorption oscillator strength, f,  $\log(Gf)$  and the radiative decay rates, A, for all allowed electric dipole transitions among As III .

**Table 1.** Radial function parameters for for Gallium-like ions in units of  $1000 \text{ cm}^{-1}$ .

Configuration	Parameter	Ion
		As III
4s <sup>2</sup> 4p	$E_{av}$	1.9600
	$\zeta_i(r_i)$	1.9600
4s <sup>2</sup> 5p	$E_{av}$	131.9407
	$\zeta_i(r_i)$	0.4827
4s <sup>2</sup> 6p	$E_{av}$	174.2346
	$\zeta_i(r_i)$	0.1856
4s <sup>2</sup> 7p	$E_{av}$	193.3800
	$\zeta_i(r_i)$	0.0975
4s <sup>2</sup> 8p	$E_{av}$	203.9731
	$\zeta_i(r_i)$	0.0576
4s <sup>2</sup> 9p	$E_{av}$	210.4644
	$\zeta_i(r_i)$	0.0369
4s <sup>2</sup> 10p	$E_{av}$	214.7338
	$\zeta_i(r_i)$	0.0250
4s <sup>2</sup> 4f	$E_{av}$	164.1104
	$\zeta_i(r_i)$	-0.0100
4s <sup>2</sup> 5f	$E_{av}$	188.4820
	$\zeta_i(r_i)$	0.0003
4s <sup>2</sup> 6f	$E_{av}$	201.0537
	$\zeta_i(r_i)$	0.0002

**Table 1. continue**

Configuration	Parameter	Ion
		As III
4s <sup>2</sup> 7f	E <sub>av</sub>	208.5886
	ζ <sub>i</sub> (r <sub>i</sub> )	0.0001
4s <sup>2</sup> 8f	E <sub>av</sub>	213.4606
	ζ <sub>i</sub> (r <sub>i</sub> )	0.0001
4s <sup>2</sup> 9f	E <sub>av</sub>	216.7884
	ζ <sub>i</sub> (r <sub>i</sub> )	0.0000
4s <sup>2</sup> 10f	E <sub>av</sub>	219.1616
	ζ <sub>i</sub> (r <sub>i</sub> )	0.0000
4s <sup>2</sup> 5s	E <sub>av</sub>	106.6940
4s <sup>2</sup> 6s	E <sub>av</sub>	162.8890
4s <sup>2</sup> 7s	E <sub>av</sub>	184.1295
4s <sup>2</sup> 8s	E <sub>av</sub>	200.8780
4s <sup>2</sup> 9s	E <sub>av</sub>	208.5050
4s <sup>2</sup> 10s	E <sub>av</sub>	213.4160
4s <sup>2</sup> 4d	E <sub>av</sub>	117.7068
	ζ <sub>i</sub> (r <sub>i</sub> )	0.0372
4s <sup>2</sup> 5d	E <sub>av</sub>	165.6740
	ζ <sub>i</sub> (r <sub>i</sub> )	0.0340
4s <sup>2</sup> 6d	E <sub>av</sub>	189.2677
	ζ <sub>i</sub> (r <sub>i</sub> )	0.0130
4s <sup>2</sup> 7d	E <sub>av</sub>	201.5790
	ζ <sub>i</sub> (r <sub>i</sub> )	0.0075
4s <sup>2</sup> 8d	E <sub>av</sub>	208.9466
	ζ <sub>i</sub> (r <sub>i</sub> )	0.0047
4s <sup>2</sup> 9d	E <sub>av</sub>	213.7121
	ζ <sub>i</sub> (r <sub>i</sub> )	0.0031
4s <sup>2</sup> 10d	E <sub>av</sub>	216.9712
	ζ <sub>i</sub> (r <sub>i</sub> )	0.0022

**Table 2.** Energy levels in cm<sup>-1</sup> for As III calculated by COWAN code in Comparison with NIST experimental values

Levels	Energy	NIST	Dev. % Relative to NIST
4s <sup>2</sup> 4p( <sup>2</sup> P <sub>1/2</sub> )	0.00	0.00	0
4s <sup>2</sup> 4p( <sup>2</sup> P <sub>3/2</sub> )	2940.00	2940.00	0
4s <sup>2</sup> 5s( <sup>2</sup> S <sub>1/2</sub> )	106694.00	106694.00	0
4s <sup>2</sup> 4d( <sup>2</sup> D <sub>3/2</sub> )	117651.00	117651.00	0
4s <sup>2</sup> 4d( <sup>2</sup> D <sub>5/2</sub> )	117744.00	117744.00	0
4s <sup>2</sup> 5p( <sup>2</sup> P <sub>1/2</sub> )	131458.00	131458.00	0
4s <sup>2</sup> 5p( <sup>2</sup> P <sub>3/2</sub> )	132182.10	132182.00	-7.57E-05
4s <sup>2</sup> 6s( <sup>2</sup> S <sub>1/2</sub> )	162889.50	162889.50	0
4s <sup>2</sup> 4f( <sup>2</sup> F <sub>7/2</sub> )	164095.40	164107.00	7.07E-03
4s <sup>2</sup> 4f( <sup>2</sup> F <sub>5/2</sub> )	164130.40	164115.00	-9.38E-03
4s <sup>2</sup> 5d( <sup>2</sup> D <sub>3/2</sub> )	165623.00	165623.00	0
4s <sup>2</sup> 5d( <sup>2</sup> D <sub>5/2</sub> )	165708.00	165708.00	0
4s <sup>2</sup> 6p( <sup>2</sup> P <sub>1/2</sub> )	174049.00		
4s <sup>2</sup> 6p( <sup>2</sup> P <sub>3/2</sub> )	174327.40		
4s <sup>2</sup> 7s( <sup>2</sup> S <sub>1/2</sub> )	184129.50		
4s <sup>2</sup> 5f( <sup>2</sup> F <sub>5/2</sub> )	188481.40		
4s <sup>2</sup> 5f( <sup>2</sup> F <sub>7/2</sub> )	188482.50		
4s <sup>2</sup> 6d( <sup>2</sup> D <sub>3/2</sub> )	189248.20		
4s <sup>2</sup> 6d( <sup>2</sup> D <sub>5/2</sub> )	189280.70		
4s <sup>2</sup> 7p( <sup>2</sup> P <sub>1/2</sub> )	193282.50		
4s <sup>2</sup> 7p( <sup>2</sup> P <sub>3/2</sub> )	193428.80		
4s <sup>2</sup> 8s( <sup>2</sup> S <sub>1/2</sub> )	200878.90		

Table 2. continue

Levels	Energy	NIST	Dev. % Relative to NIST
4s <sup>2</sup> 6f( <sup>2</sup> F <sub>5/2</sub> )	201053.30		
4s <sup>2</sup> 6f( <sup>2</sup> F <sub>7/2</sub> )	201054.00		
4s <sup>2</sup> 7d( <sup>2</sup> D <sub>3/2</sub> )	201567.80		
4s <sup>2</sup> 7d( <sup>2</sup> D <sub>5/2</sub> )	201586.50		
4s <sup>2</sup> 8p( <sup>2</sup> P <sub>1/2</sub> )	203915.50		
4s <sup>2</sup> 8p( <sup>2</sup> P <sub>3/2</sub> )	204001.90		
4s <sup>2</sup> 9s( <sup>2</sup> S <sub>1/2</sub> )	208505.20		
4s <sup>2</sup> 7f( <sup>2</sup> F <sub>5/2</sub> )	208588.40		
4s <sup>2</sup> 7f( <sup>2</sup> F <sub>7/2</sub> )	208588.80		
4s <sup>2</sup> 8d( <sup>2</sup> D <sub>3/2</sub> )	208939.50		
4s <sup>2</sup> 8d( <sup>2</sup> D <sub>5/2</sub> )	208951.30		
4s <sup>2</sup> 9p( <sup>2</sup> P <sub>1/2</sub> )	210427.50		
4s <sup>2</sup> 9p( <sup>2</sup> P <sub>3/2</sub> )	210482.90		
4s <sup>2</sup> 10s( <sup>2</sup> S <sub>1/2</sub> )	213416.60		
4s <sup>2</sup> 8f( <sup>2</sup> F <sub>5/2</sub> )	213460.40		
4s <sup>2</sup> 8f( <sup>2</sup> F <sub>7/2</sub> )	213460.70		
4s <sup>2</sup> 9d( <sup>2</sup> D <sub>3/2</sub> )	213707.40		
4s <sup>2</sup> 9d( <sup>2</sup> D <sub>5/2</sub> )	213715.20		
4s <sup>2</sup> 10p( <sup>2</sup> P <sub>1/2</sub> )	214708.80		
4s <sup>2</sup> 10p( <sup>2</sup> P <sub>3/2</sub> )	214746.30		
4s <sup>2</sup> 9f( <sup>2</sup> F <sub>5/2</sub> )	216788.40		
4s <sup>2</sup> 9f( <sup>2</sup> F <sub>7/2</sub> )	216788.40		
4s <sup>2</sup> 10d( <sup>2</sup> D <sub>3/2</sub> )	216967.90		
4s <sup>2</sup> 10d( <sup>2</sup> D <sub>5/2</sub> )	216973.40		
4s <sup>2</sup> 10f( <sup>2</sup> F <sub>5/2</sub> )	219161.60		
4s <sup>2</sup> 10f( <sup>2</sup> F <sub>7/2</sub> )	219161.60		

Table 3. Wavelengths, log gf, oscillator strengths and radiative decay rates for As III.

$\lambda$ (Å)	upper levels	lower levels	Log(G f)	f	A(s <sup>-1</sup> )
460.90	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>1/2</sub> )	-2.330	2.34E-03	3.68E+07
467.22	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>3/2</sub> )	-2.081	2.07E-03	4.23E+07
467.23	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>3/2</sub> )	-3.035	2.30E-04	7.05E+06
467.93	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>1/2</sub> )	-2.145	3.58E-03	5.45E+07
468.57	4s <sup>2</sup> 10s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>1/2</sub> )	-2.494	1.60E-03	4.87E+07
474.44	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>3/2</sub> )	-1.896	3.17E-03	6.28E+07
474.46	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>3/2</sub> )	-2.850	3.53E-04	1.05E+07
475.11	4s <sup>2</sup> 10s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>3/2</sub> )	-2.199	1.58E-03	9.35E+07
478.61	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>1/2</sub> )	-1.925	5.94E-03	8.65E+07
479.60	4s <sup>2</sup> 9s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>1/2</sub> )	-2.296	2.53E-03	7.35E+07
485.41	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>3/2</sub> )	-1.676	5.27E-03	9.95E+07
485.44	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>3/2</sub> )	-2.630	5.85E-04	1.66E+07
486.46	4s <sup>2</sup> 9s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>3/2</sub> )	-2.002	2.49E-03	1.41E+08
496.11	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>1/2</sub> )	-1.652	1.11E-02	1.51E+08
497.81	4s <sup>2</sup> 8s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>1/2</sub> )	-2.057	4.38E-03	1.18E+08
503.41	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>3/2</sub> )	-1.403	9.88E-03	1.73E+08
503.45	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>3/2</sub> )	-2.358	1.10E-03	2.90E+07
505.21	4s <sup>2</sup> 8s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>3/2</sub> )	-1.763	4.31E-03	2.26E+08
528.41	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>1/2</sub> )	-1.289	2.57E-02	3.08E+08
536.65	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>3/2</sub> )	-1.040	2.28E-02	3.52E+08
536.75	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>3/2</sub> )	-1.994	2.53E-03	5.88E+07
543.10	4s <sup>2</sup> 7s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>1/2</sub> )	-1.762	8.64E-03	1.96E+08
551.91	4s <sup>2</sup> 7s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>3/2</sub> )	-1.468	8.51E-03	3.73E+08
603.78	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>1/2</sub> )	-0.747	8.95E-02	8.20E+08
613.91	4s <sup>2</sup> 6s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>1/2</sub> )	-1.325	2.36E-02	4.19E+08

Table 3. continue

$\lambda$ (Å)	upper levels	lower levels	Log(G f)	f	A(s <sup>-1</sup> )
614.37	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>3/2</sub> )	-0.499	7.92E-02	9.33E+08
614.69	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>3/2</sub> )	-1.453	8.80E-03	1.55E+08
625.20	4s <sup>2</sup> 6s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>3/2</sub> )	-1.031	2.33E-02	7.95E+08
849.97	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>1/2</sub> )	0.354	1.13E+00	5.23E+09
871.05	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>3/2</sub> )	0.599	9.93E-01	5.82E+09
871.76	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>3/2</sub> )	-0.356	1.10E-01	9.68E+08
925.48	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 5s( <sup>2</sup> S <sub>1/2</sub> )	-3.699	9.98E-05	3.90E+05
925.80	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 5s( <sup>2</sup> S <sub>1/2</sub> )	-4.000	4.99E-05	3.89E+05
937.26	4s <sup>2</sup> 5s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>1/2</sub> )	-0.524	1.50E-01	1.14E+09
963.50	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 5s( <sup>2</sup> S <sub>1/2</sub> )	-3.596	1.27E-04	4.55E+05
963.82	4s <sup>2</sup> 5s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 4p( <sup>2</sup> P <sub>3/2</sub> )	-0.235	1.46E-01	2.09E+09
964.01	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 5s( <sup>2</sup> S <sub>1/2</sub> )	-3.897	6.33E-05	4.55E+05
985.12	4s <sup>2</sup> 10f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>3/2</sub> )	-1.713	4.84E-03	2.22E+07
986.02	4s <sup>2</sup> 10f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>5/2</sub> )	-2.859	2.30E-04	1.58E+06
986.02	4s <sup>2</sup> 10f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>5/2</sub> )	-1.558	4.61E-03	2.38E+07
1008.70	4s <sup>2</sup> 9f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>3/2</sub> )	-1.536	7.27E-03	3.18E+07
1009.65	4s <sup>2</sup> 9f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>5/2</sub> )	-2.682	3.46E-04	2.27E+06
1009.65	4s <sup>2</sup> 9f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>5/2</sub> )	-1.381	6.93E-03	3.40E+07
1027.67	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 5s( <sup>2</sup> S <sub>1/2</sub> )	-3.541	1.44E-04	4.55E+05
1028.58	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 5s( <sup>2</sup> S <sub>1/2</sub> )	-3.842	7.18E-05	4.53E+05
1029.92	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>3/2</sub> )	-3.733	4.62E-05	2.90E+05
1030.31	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>3/2</sub> )	-3.035	2.30E-04	2.90E+06
1030.90	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>5/2</sub> )	-2.780	2.76E-04	2.60E+06
1043.74	4s <sup>2</sup> 8f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>3/2</sub> )	-1.326	1.18E-02	4.82E+07
1044.75	4s <sup>2</sup> 8f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>5/2</sub> )	-1.171	1.12E-02	5.15E+07
1044.75	4s <sup>2</sup> 8f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>5/2</sub> )	-2.472	5.62E-04	3.43E+06
1077.22	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>3/2</sub> )	-3.536	7.27E-05	4.18E+05
1077.86	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>3/2</sub> )	-2.837	3.63E-04	4.18E+06
1078.30	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>5/2</sub> )	-2.582	4.36E-04	3.75E+06
1099.66	4s <sup>2</sup> 7f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>3/2</sub> )	-1.067	2.14E-02	7.87E+07
1100.78	4s <sup>2</sup> 7f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>5/2</sub> )	-0.913	2.04E-02	8.41E+07
1100.78	4s <sup>2</sup> 7f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>5/2</sub> )	-2.214	1.02E-03	5.60E+06
1152.94	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 5s( <sup>2</sup> S <sub>1/2</sub> )	-3.783	8.23E-05	2.07E+05
1154.89	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 5s( <sup>2</sup> S <sub>1/2</sub> )	-4.085	4.10E-05	2.06E+05
1158.07	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>3/2</sub> )	-3.295	1.27E-04	6.30E+05
1159.23	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>3/2</sub> )	-2.596	6.33E-04	6.30E+06
1159.31	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>5/2</sub> )	-2.341	7.59E-04	5.65E+06
1169.46	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>1/2</sub> )	-1.951	5.59E-03	1.36E+07
1179.37	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>3/2</sub> )	-1.700	4.98E-03	1.60E+07
1179.44	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>3/2</sub> )	-2.654	5.54E-04	2.65E+06
1199.01	4s <sup>2</sup> 6f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>3/2</sub> )	-0.732	4.63E-02	1.44E+08
1200.34	4s <sup>2</sup> 6f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>5/2</sub> )	-0.577	4.41E-02	1.54E+08
1200.35	4s <sup>2</sup> 6f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>5/2</sub> )	-1.878	2.21E-03	1.02E+07
1215.81	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>1/2</sub> )	-1.739	9.11E-03	2.06E+07
1220.13	4s <sup>2</sup> 10s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>1/2</sub> )	-2.172	3.36E-03	1.51E+07
1226.50	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>3/2</sub> )	-1.488	8.12E-03	2.40E+07
1226.61	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>3/2</sub> )	-2.442	9.03E-04	4.00E+06
1231.00	4s <sup>2</sup> 10s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>3/2</sub> )	-1.875	3.33E-03	2.94E+07
1290.63	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>1/2</sub> )	-1.476	1.67E-02	3.35E+07
1297.91	4s <sup>2</sup> 9s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>1/2</sub> )	-1.934	5.82E-03	2.31E+07
1302.61	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>3/2</sub> )	-1.224	1.49E-02	3.92E+07
1302.80	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>3/2</sub> )	-2.179	1.65E-03	6.53E+06
1310.22	4s <sup>2</sup> 9s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>3/2</sub> )	-1.637	5.76E-03	4.48E+07
1319.65	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>3/2</sub> )	-2.979	2.62E-04	1.01E+06
1321.27	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>5/2</sub> )	-2.025	1.57E-03	9.03E+06
1322.20	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>3/2</sub> )	-2.281	1.31E-03	1.00E+07

Table 3. continue

$\lambda$ (Å)	upper levels	lower levels	Log(G f)	f	A(s <sup>-1</sup> )
1411.82	4s <sup>2</sup> 5f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>3/2</sub> )	-0.253	1.40E-01	3.12E+08
1413.66	4s <sup>2</sup> 5f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>5/2</sub> )	-0.098	1.33E-01	3.33E+08
1413.68	4s <sup>2</sup> 5f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>5/2</sub> )	-1.400	6.63E-03	2.22E+07
1426.34	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>1/2</sub> )	-1.126	3.74E-02	6.13E+07
1440.49	4s <sup>2</sup> 8s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>1/2</sub> )	-1.625	1.18E-02	3.81E+07
1440.83	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>3/2</sub> )	-0.876	3.32E-02	7.13E+07
1441.22	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>3/2</sub> )	-1.830	3.69E-03	1.19E+07
1455.67	4s <sup>2</sup> 8s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>3/2</sub> )	-1.329	1.17E-02	7.40E+07
1478.56	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 5s( <sup>2</sup> S <sub>1/2</sub> )	-3.048	4.47E-04	6.83E+05
1484.67	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 5s( <sup>2</sup> S <sub>1/2</sub> )	-3.350	2.23E-04	6.75E+05
1730.40	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>1/2</sub> )	-0.609	1.23E-01	1.37E+08
1751.36	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>3/2</sub> )	-0.359	1.09E-01	1.59E+08
1752.35	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>3/2</sub> )	-1.313	1.22E-02	2.65E+07
1764.40	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>3/2</sub> )	-2.493	8.03E-04	1.72E+06
1767.30	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>5/2</sub> )	-1.539	4.81E-03	1.54E+07
1773.11	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>3/2</sub> )	-1.796	4.00E-03	1.70E+07
1867.81	4s <sup>2</sup> 10f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>3/2</sub> )	-1.311	1.22E-02	1.56E+07
1870.78	4s <sup>2</sup> 10f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>5/2</sub> )	-2.458	5.80E-04	1.11E+06
1870.78	4s <sup>2</sup> 10f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>5/2</sub> )	-1.157	1.16E-02	1.66E+07
1891.15	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 4f( <sup>2</sup> F <sub>7/2</sub> )	-3.420	4.75E-05	1.18E+05
1892.60	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 4f( <sup>2</sup> F <sub>5/2</sub> )	-3.575	4.43E-05	1.24E+05
1898.56	4s <sup>2</sup> 7s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>1/2</sub> )	-1.206	3.11E-02	5.75E+07
1925.02	4s <sup>2</sup> 7s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>3/2</sub> )	-0.911	3.07E-02	1.11E+08
1928.39	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 6s( <sup>2</sup> S <sub>1/2</sub> )	-3.802	7.88E-05	7.08E+04
1929.78	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 6s( <sup>2</sup> S <sub>1/2</sub> )	-4.104	3.93E-05	7.05E+04
1954.45	4s <sup>2</sup> 9f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>3/2</sub> )	-1.113	1.93E-02	2.25E+07
1957.70	4s <sup>2</sup> 9f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>5/2</sub> )	-2.260	9.15E-04	1.60E+06
1957.70	4s <sup>2</sup> 9f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>5/2</sub> )	-0.959	1.83E-02	2.39E+07
2015.33	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 4f( <sup>2</sup> F <sub>7/2</sub> )	-3.155	8.74E-05	1.92E+05
2017.06	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 4f( <sup>2</sup> F <sub>5/2</sub> )	-3.310	8.15E-05	2.01E+05
2035.69	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>3/2</sub> )	-3.530	7.37E-05	1.19E+05
2037.25	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>3/2</sub> )	-2.831	3.68E-04	1.19E+06
2039.22	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>5/2</sub> )	-2.576	4.42E-04	1.06E+06
2090.42	4s <sup>2</sup> 8f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>3/2</sub> )	-0.871	3.36E-02	3.42E+07
2094.12	4s <sup>2</sup> 8f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>5/2</sub> )	-0.717	3.20E-02	3.65E+07
2094.14	4s <sup>2</sup> 8f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>5/2</sub> )	-2.018	1.60E-03	2.43E+06
2101.13	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 6s( <sup>2</sup> S <sub>1/2</sub> )	-3.901	6.27E-05	4.75E+04
2152.42	4s <sup>2</sup> 4f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>3/2</sub> )	0.572	9.33E-01	8.97E+08
2155.80	4s <sup>2</sup> 4f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>5/2</sub> )	-0.575	4.43E-02	6.37E+07
2157.43	4s <sup>2</sup> 4f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>5/2</sub> )	0.726	8.87E-01	9.53E+08
2229.17	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>3/2</sub> )	-3.292	1.27E-04	1.72E+05
2229.36	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 4f( <sup>2</sup> F <sub>7/2</sub> )	-2.809	1.94E-04	3.47E+05
2231.10	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 4f( <sup>2</sup> F <sub>5/2</sub> )	-4.111	1.29E-05	1.73E+04
2231.69	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 4f( <sup>2</sup> F <sub>5/2</sub> )	-2.965	1.80E-04	3.63E+05
2231.92	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>3/2</sub> )	-2.593	6.37E-04	1.71E+06
2233.40	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>5/2</sub> )	-2.338	7.65E-04	1.54E+06
2327.45	4s <sup>2</sup> 7f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>3/2</sub> )	-0.561	6.87E-02	5.65E+07
2329.98	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>1/2</sub> )	-1.604	1.24E-02	7.65E+06
2332.05	4s <sup>2</sup> 7f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>5/2</sub> )	-0.407	6.53E-02	6.01E+07
2332.07	4s <sup>2</sup> 7f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>5/2</sub> )	-1.708	3.26E-03	4.00E+06
2344.89	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>3/2</sub> )	-1.351	1.11E-02	9.00E+06
2345.19	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>3/2</sub> )	-2.306	1.23E-03	1.50E+06
2521.53	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>1/2</sub> )	-1.349	2.24E-02	1.18E+07
2538.86	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>3/2</sub> )	-1.096	2.00E-02	1.38E+07
2539.36	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>3/2</sub> )	-2.051	2.22E-03	2.30E+06
2540.16	4s <sup>2</sup> 10s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>1/2</sub> )	-1.820	7.56E-03	7.80E+06

Table 3. continue

$\lambda$ (Å)	upper levels	lower levels	Log(G f)	f	A(s <sup>-1</sup> )
2558.25	4s <sup>2</sup> 10s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>3/2</sub> )	-1.522	7.51E-03	1.53E+07
2605.60	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>3/2</sub> )	-2.972	2.66E-04	2.63E+05
2611.38	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>5/2</sub> )	-2.018	1.60E-03	2.35E+06
2611.48	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>3/2</sub> )	-2.274	1.33E-03	2.61E+06
2667.30	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 4f( <sup>2</sup> F <sub>7/2</sub> )	-2.324	5.92E-04	7.42E+05
2669.79	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 4f( <sup>2</sup> F <sub>5/2</sub> )	-3.625	3.95E-05	3.70E+04
2671.13	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 4f( <sup>2</sup> F <sub>5/2</sub> )	-2.479	5.53E-04	7.75E+05
2822.44	4s <sup>2</sup> 6f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>3/2</sub> )	-0.124	1.88E-01	1.05E+08
2829.17	4s <sup>2</sup> 6f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>5/2</sub> )	0.030	1.79E-01	1.12E+08
2829.23	4s <sup>2</sup> 6f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>5/2</sub> )	-1.271	8.93E-03	7.43E+06
2866.11	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>1/2</sub> )	-1.012	4.86E-02	1.98E+07
2888.18	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>3/2</sub> )	-0.760	4.34E-02	2.32E+07
2889.16	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>3/2</sub> )	-1.714	4.83E-03	3.85E+06
2902.24	4s <sup>2</sup> 9s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>1/2</sub> )	-1.510	1.54E-02	1.22E+07
2925.88	4s <sup>2</sup> 9s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>3/2</sub> )	-1.213	1.53E-02	2.39E+07
2926.97	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>1/2</sub> )	0.393	1.24E+00	4.83E+08
2982.76	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>3/2</sub> )	0.640	1.09E+00	5.47E+08
2990.35	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>3/2</sub> )	-0.315	1.21E-01	9.03E+07
3181.52	4s <sup>2</sup> 6s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>1/2</sub> )	-0.293	2.55E-01	1.68E+08
3256.54	4s <sup>2</sup> 6s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>3/2</sub> )	-0.002	2.49E-01	3.13E+08
3274.48	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 6s( <sup>2</sup> S <sub>1/2</sub> )	-2.464	1.72E-03	5.35E+05
3290.23	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 6s( <sup>2</sup> S <sub>1/2</sub> )	-2.767	8.54E-04	5.25E+05
3342.98	4s <sup>2</sup> 10f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>3/2</sub> )	-1.026	2.35E-02	9.37E+06
3346.62	4s <sup>2</sup> 10f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>5/2</sub> )	-2.172	1.12E-03	6.67E+05
3346.62	4s <sup>2</sup> 10f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>5/2</sub> )	-0.871	2.24E-02	1.00E+07
3509.89	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 5f( <sup>2</sup> F <sub>7/2</sub> )	-2.626	2.95E-04	2.13E+05
3510.44	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 5f( <sup>2</sup> F <sub>5/2</sub> )	-2.781	2.76E-04	2.24E+05
3596.38	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>3/2</sub> )	-2.447	8.92E-04	4.60E+05
3607.41	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>5/2</sub> )	-1.494	5.34E-03	4.10E+06
3615.39	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>3/2</sub> )	-1.751	4.43E-03	4.53E+06
3631.06	4s <sup>2</sup> 9f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>3/2</sub> )	-0.795	4.01E-02	1.35E+07
3633.89	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>1/2</sub> )	-0.514	1.53E-01	3.88E+07
3635.35	4s <sup>2</sup> 9f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>5/2</sub> )	-1.942	1.90E-03	9.62E+05
3635.35	4s <sup>2</sup> 9f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>5/2</sub> )	-0.641	3.81E-02	1.44E+07
3668.50	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>3/2</sub> )	-0.263	1.36E-01	4.50E+07
3671.03	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>3/2</sub> )	-1.218	1.51E-02	7.50E+06
3727.19	4s <sup>2</sup> 8s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>1/2</sub> )	-1.054	4.41E-02	2.12E+07
3766.27	4s <sup>2</sup> 8s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>3/2</sub> )	-0.757	4.37E-02	4.12E+07
3921.86	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>3/2</sub> )	-3.349	1.12E-04	4.85E+04
3923.41	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 5s( <sup>2</sup> S <sub>1/2</sub> )	0.281	9.55E-01	2.07E+08
3926.87	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>5/2</sub> )	-2.395	6.71E-04	4.35E+05
3927.64	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>3/2</sub> )	-2.650	5.59E-04	4.84E+05
3962.94	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 5f( <sup>2</sup> F <sub>5/2</sub> )	-3.599	4.19E-05	1.78E+04
3963.10	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 5f( <sup>2</sup> F <sub>7/2</sub> )	-2.298	6.29E-04	3.57E+05
3964.16	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 5f( <sup>2</sup> F <sub>5/2</sub> )	-2.453	5.87E-04	3.75E+05
3970.57	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 4f(2F <sub>7/2</sub> )	-1.526	3.72E-03	2.10E+06
3976.10	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 4f( <sup>2</sup> F <sub>5/2</sub> )	-2.828	2.47E-04	1.04E+05
3981.24	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 4f( <sup>2</sup> F <sub>5/2</sub> )	-1.682	3.46E-03	2.19E+06
4038.12	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 5s( <sup>2</sup> S <sub>1/2</sub> )	-0.033	4.63E-01	1.90E+08
4130.15	4s <sup>2</sup> 8f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>3/2</sub> )	-0.499	7.92E-02	2.07E+07
4135.64	4s <sup>2</sup> 8f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>5/2</sub> )	-0.345	7.53E-02	2.20E+07
4135.70	4s <sup>2</sup> 8f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>5/2</sub> )	-1.646	3.76E-03	1.47E+06
4222.01	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>1/2</sub> )	-1.251	2.80E-02	5.25E+06
4247.25	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>3/2</sub> )	-0.998	2.51E-02	6.18E+06
4248.24	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>3/2</sub> )	-1.952	2.79E-03	1.03E+06
4374.76	4s <sup>2</sup> 5f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>3/2</sub> )	0.610	1.02E+00	2.37E+08

Table 3. continue

$\lambda$ (Å)	upper levels	lower levels	Log(G f)	f	A(s <sup>-1</sup> )
4390.89	4s <sup>2</sup> 5f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>5/2</sub> )	0.764	9.68E-01	2.51E+08
4391.09	4s <sup>2</sup> 5f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>5/2</sub> )	-0.537	4.84E-02	1.67E+07
4709.28	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>3/2</sub> )	-3.023	2.37E-04	7.15E+04
4716.50	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>5/2</sub> )	-2.069	1.42E-03	6.40E+05
4721.59	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>3/2</sub> )	-2.325	1.18E-03	7.10E+05
4885.22	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 5f( <sup>2</sup> F <sub>5/2</sub> )	-3.143	1.20E-04	3.35E+04
4885.47	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 5f( <sup>2</sup> F <sub>7/2</sub> )	-1.842	1.80E-03	6.70E+05
4888.03	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 5f( <sup>2</sup> F <sub>5/2</sub> )	-1.997	1.68E-03	7.03E+05
4895.97	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>1/2</sub> )	-0.921	6.00E-02	8.35E+06
4929.40	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>3/2</sub> )	-0.669	5.36E-02	9.80E+06
4931.28	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>3/2</sub> )	-1.623	5.95E-03	1.63E+06
4966.70	4s <sup>2</sup> 10s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>1/2</sub> )	-1.411	1.94E-02	5.25E+06
5003.04	4s <sup>2</sup> 10s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>3/2</sub> )	-1.113	1.93E-02	1.03E+07
5032.11	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 7s( <sup>2</sup> S <sub>1/2</sub> )	-2.074	4.21E-03	5.55E+05
5054.08	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 7s( <sup>2</sup> S <sub>1/2</sub> )	-2.377	2.10E-03	5.50E+05
5170.58	4s <sup>2</sup> 7f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>3/2</sub> )	-0.087	2.05E-01	3.40E+07
5179.19	4s <sup>2</sup> 7f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>5/2</sub> )	0.068	1.95E-01	3.64E+07
5179.28	4s <sup>2</sup> 7f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>5/2</sub> )	-1.234	9.72E-03	2.42E+06
5683.80	4s <sup>2</sup> 10f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>3/2</sub> )	-0.741	4.54E-02	6.25E+06
5689.87	4s <sup>2</sup> 10f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>5/2</sub> )	-1.887	2.16E-03	4.45E+05
5689.87	4s <sup>2</sup> 10f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>5/2</sub> )	-0.586	4.32E-02	6.68E+06
6281.64	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 6f( <sup>2</sup> F <sub>7/2</sub> )	-1.990	1.28E-03	2.88E+05
6283.54	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 6f( <sup>2</sup> F <sub>5/2</sub> )	-2.145	1.19E-03	3.03E+05
6386.90	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>1/2</sub> )	-0.435	1.84E-01	1.50E+07
6442.24	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>3/2</sub> )	-0.184	1.64E-01	1.75E+07
6447.12	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>3/2</sub> )	-1.139	1.81E-02	2.93E+06
6569.14	4s <sup>2</sup> 9s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>1/2</sub> )	-0.950	5.61E-02	8.70E+06
6570.02	4s <sup>2</sup> 9f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>3/2</sub> )	-0.454	8.79E-02	9.05E+06
6578.13	4s <sup>2</sup> 9f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>5/2</sub> )	-1.601	4.17E-03	6.45E+05
6578.13	4s <sup>2</sup> 9f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>5/2</sub> )	-0.300	8.35E-02	9.66E+06
6579.29	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>1/2</sub> )	0.448	1.40E+00	1.08E+08
6632.86	4s <sup>2</sup> 9s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>3/2</sub> )	-0.653	5.56E-02	1.69E+07
6687.49	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>3/2</sub> )	0.696	1.24E+00	1.23E+08
6702.05	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>3/2</sub> )	-0.259	1.38E-01	2.04E+07
6777.96	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>3/2</sub> )	-2.465	8.56E-04	1.25E+05
6792.93	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>5/2</sub> )	-1.512	5.12E-03	1.11E+06
6817.89	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>3/2</sub> )	-1.769	4.25E-03	1.22E+06
6881.82	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>3/2</sub> )	-1.025	2.36E-02	3.33E+06
6926.14	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>5/2</sub> )	-0.074	1.41E-01	2.93E+07
7242.70	4s <sup>2</sup> 5p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 4d( <sup>2</sup> D <sub>3/2</sub> )	-0.348	1.12E-01	2.85E+07
7598.90	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>5/2</sub> )	-2.113	1.28E-03	2.23E+05
7609.74	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>3/2</sub> )	-2.369	1.07E-03	2.47E+05
7630.62	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 5f( <sup>2</sup> F <sub>5/2</sub> )	-2.411	6.46E-04	7.42E+04
7631.23	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 5f( <sup>2</sup> F <sub>7/2</sub> )	-1.110	9.70E-03	1.48E+06
7641.55	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 5f( <sup>2</sup> F <sub>5/2</sub> )	-1.266	9.03E-03	1.55E+06
7661.43	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>1/2</sub> )	-0.851	7.04E-02	4.00E+06
7709.21	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>3/2</sub> )	-0.598	6.31E-02	4.72E+06
7712.48	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>3/2</sub> )	-1.552	7.01E-03	7.85E+05
7897.71	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 6f( <sup>2</sup> F <sub>5/2</sub> )	-2.856	2.32E-04	2.48E+04
7898.15	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 6f( <sup>2</sup> F <sub>7/2</sub> )	-1.555	3.48E-03	4.97E+05
7902.55	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 6f( <sup>2</sup> F <sub>5/2</sub> )	-1.710	3.25E-03	5.20E+05
8408.55	4s <sup>2</sup> 8f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>3/2</sub> )	-0.053	2.21E-01	1.39E+07
8421.58	4s <sup>2</sup> 8f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>5/2</sub> )	0.101	2.10E-01	1.49E+07
8421.83	4s <sup>2</sup> 8f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>5/2</sub> )	-1.200	1.05E-02	9.88E+05
8470.91	4s <sup>2</sup> 6f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>3/2</sub> )	0.607	1.01E+00	6.27E+07
8493.80	4s <sup>2</sup> 6f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>5/2</sub> )	0.761	9.62E-01	6.66E+07

Table 3. continue

$\lambda$ (Å)	upper levels	lower levels	Log(G f)	f	A(s <sup>-1</sup> )
8494.30	4s <sup>2</sup> 6f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>5/2</sub> )	-0.540	4.81E-02	4.43E+06
8742.86	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 6s( <sup>2</sup> S <sub>1/2</sub> )	0.422	1.32E+00	5.78E+07
8960.98	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 6s( <sup>2</sup> S <sub>1/2</sub> )	0.110	6.44E-01	5.35E+07
9782.77	4s <sup>2</sup> 10f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>3/2</sub> )	-0.419	9.52E-02	4.43E+06
9794.03	4s <sup>2</sup> 10f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>5/2</sub> )	-1.565	4.53E-03	3.15E+05
9794.03	4s <sup>2</sup> 10f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>5/2</sub> )	-0.264	9.07E-02	4.74E+06
9920.14	4s <sup>2</sup> 7s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>1/2</sub> )	-0.276	2.65E-01	1.80E+07
10201.90	4s <sup>2</sup> 7s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>3/2</sub> )	0.013	2.58E-01	3.30E+07
10212.47	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>1/2</sub> )	-0.372	2.12E-01	6.78E+06
10295.16	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>3/2</sub> )	-0.120	1.90E-01	7.95E+06
10303.38	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>3/2</sub> )	-1.075	2.10E-02	1.32E+06
10412.38	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 8s( <sup>2</sup> S <sub>1/2</sub> )	-1.961	5.47E-03	1.68E+05
10472.74	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 8s( <sup>2</sup> S <sub>1/2</sub> )	-2.265	2.71E-03	1.66E+05
10525.10	4s <sup>2</sup> 10s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>1/2</sub> )	-0.866	6.80E-02	4.10E+06
10621.69	4s <sup>2</sup> 10s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>3/2</sub> )	-0.569	6.74E-02	8.00E+06
10753.55	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 7s( <sup>2</sup> S <sub>1/2</sub> )	0.709	2.56E+00	7.38E+07
10925.38	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 7s( <sup>2</sup> S <sub>1/2</sub> )	0.401	1.26E+00	7.05E+07
11216.92	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>3/2</sub> )	-2.473	8.40E-04	4.45E+04
11240.57	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>5/2</sub> )	-1.520	5.03E-03	4.00E+05
11287.00	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>3/2</sub> )	-1.777	4.17E-03	4.38E+05
11488.44	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>3/2</sub> )	-0.597	6.32E-02	3.20E+06
11601.74	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>5/2</sub> )	0.353	3.76E-01	2.80E+07
11868.03	4s <sup>2</sup> 6p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>3/2</sub> )	0.088	3.06E-01	2.90E+07
11926.06	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 7f( <sup>2</sup> F <sub>5/2</sub> )	-2.654	3.69E-04	1.73E+04
11926.56	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 7f( <sup>2</sup> F <sub>7/2</sub> )	-1.353	5.54E-03	3.47E+05
11933.89	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 7f( <sup>2</sup> F <sub>5/2</sub> )	-1.508	5.17E-03	3.63E+05
12069.64	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>1/2</sub> )	0.503	1.59E+00	3.65E+07
12258.28	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>3/2</sub> )	0.752	1.41E+00	4.18E+07
12286.52	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>3/2</sub> )	-0.204	1.56E-01	6.93E+06
12661.43	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 6f( <sup>2</sup> F <sub>5/2</sub> )	-2.162	1.15E-03	4.77E+04
12662.56	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 6f( <sup>2</sup> F <sub>7/2</sub> )	-0.861	1.72E-02	9.55E+05
12680.30	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 6f( <sup>2</sup> F <sub>5/2</sub> )	-1.017	1.60E-02	9.98E+05
12740.72	4s <sup>2</sup> 9f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>3/2</sub> )	-0.025	2.36E-01	6.47E+06
12759.82	4s <sup>2</sup> 9f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>5/2</sub> )	0.129	2.24E-01	6.90E+06
12759.82	4s <sup>2</sup> 9f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>5/2</sub> )	-1.172	1.12E-02	4.60E+05
13164.13	4s <sup>2</sup> 8s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>1/2</sub> )	-0.014	4.84E-01	1.87E+07
13422.55	4s <sup>2</sup> 8s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>3/2</sub> )	0.279	4.75E-01	3.52E+07
14243.69	4s <sup>2</sup> 7f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>3/2</sub> )	0.624	1.05E+00	2.30E+07
14281.12	4s <sup>2</sup> 7f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>5/2</sub> )	0.777	9.98E-01	2.45E+07
14281.84	4s <sup>2</sup> 7f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>5/2</sub> )	-0.524	4.99E-02	1.63E+06
15289.58	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>1/2</sub> )	-0.319	2.40E-01	3.43E+06
15407.01	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>3/2</sub> )	-0.067	2.14E-01	4.02E+06
15420.08	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>3/2</sub> )	-1.022	2.38E-02	6.68E+05
16022.81	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 9s( <sup>2</sup> S <sub>1/2</sub> )	-1.813	7.68E-03	1.00E+05
16119.67	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 9s( <sup>2</sup> S <sub>1/2</sub> )	-2.116	3.82E-03	9.80E+04
17256.26	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>5/2</sub> )	-1.530	4.92E-03	1.65E+05
17333.28	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>3/2</sub> )	-1.787	4.08E-03	1.81E+05
18334.66	4s <sup>2</sup> 10f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>3/2</sub> )	0.001	2.51E-01	3.32E+06
18360.75	4s <sup>2</sup> 10f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>5/2</sub> )	0.155	2.38E-01	3.54E+06
18360.75	4s <sup>2</sup> 10f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>5/2</sub> )	-1.146	1.19E-02	2.35E+05
19505.34	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 7f( <sup>2</sup> F <sub>5/2</sub> )	-1.985	1.72E-03	3.02E+04
19506.68	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 7f( <sup>2</sup> F <sub>7/2</sub> )	-0.684	2.59E-02	6.05E+05
19534.88	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 7f( <sup>2</sup> F <sub>5/2</sub> )	-0.840	2.41E-02	6.33E+05
19904.26	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>1/2</sub> )	0.552	1.78E+00	1.50E+07
20204.47	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>3/2</sub> )	0.801	1.58E+00	1.72E+07
20252.55	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>3/2</sub> )	-0.154	1.75E-01	2.85E+06

Table 3. continue

$\lambda$ (Å)	upper levels	lower levels	Log(G f)	f	A(s <sup>-1</sup> )
21787.92	4s <sup>2</sup> 9s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>1/2</sub> )	0.079	6.00E-01	8.40E+06
22119.73	4s <sup>2</sup> 8f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>3/2</sub> )	0.644	1.10E+00	1.00E+07
22175.65	4s <sup>2</sup> 8f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>5/2</sub> )	0.798	1.05E+00	1.06E+07
22177.38	4s <sup>2</sup> 8f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>5/2</sub> )	-0.503	5.23E-02	7.10E+05
22205.94	4s <sup>2</sup> 9s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>3/2</sub> )	0.371	5.87E-01	1.59E+07
23920.30	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>3/2</sub> )	-0.468	8.51E-02	9.93E+05
24107.72	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>5/2</sub> )	0.483	5.07E-01	8.73E+06
24787.45	4s <sup>2</sup> 7p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>3/2</sub> )	0.216	4.11E-01	8.90E+06
28465.70	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 8f( <sup>2</sup> F <sub>5/2</sub> )	-1.848	2.36E-03	1.95E+04
28468.54	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 8f( <sup>2</sup> F <sub>7/2</sub> )	-0.547	3.55E-02	3.90E+05
28510.34	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 8f( <sup>2</sup> F <sub>5/2</sub> )	-0.702	3.31E-02	4.08E+05
30488.26	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>1/2</sub> )	0.596	1.97E+00	7.08E+06
30937.23	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>3/2</sub> )	0.845	1.75E+00	8.13E+06
31011.60	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>3/2</sub> )	-0.110	1.94E-01	1.35E+06
32020.48	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 8s( <sup>2</sup> S <sub>1/2</sub> )	0.543	1.75E+00	5.68E+06
32457.51	4s <sup>2</sup> 9f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>3/2</sub> )	0.665	1.16E+00	4.88E+06
32539.36	4s <sup>2</sup> 9f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>5/2</sub> )	0.819	1.10E+00	5.19E+06
32539.37	4s <sup>2</sup> 9f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>5/2</sub> )	-0.482	5.49E-02	3.47E+05
32931.57	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 8s( <sup>2</sup> S <sub>1/2</sub> )	0.230	8.49E-01	5.20E+06
33454.89	4s <sup>2</sup> 10s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>1/2</sub> )	0.155	7.14E-01	4.26E+06
34086.08	4s <sup>2</sup> 10s( <sup>2</sup> S <sub>1/2</sub> )	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>3/2</sub> )	0.448	7.01E-01	8.05E+06
41082.10	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>3/2</sub> )	-0.355	1.10E-01	4.38E+05
41401.03	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>5/2</sub> )	0.596	6.58E-01	3.85E+06
42593.99	4s <sup>2</sup> 8p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>3/2</sub> )	0.329	5.33E-01	3.92E+06
44265.40	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>1/2</sub> )	0.636	2.16E+00	3.68E+06
44901.42	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>3/2</sub> )	0.885	1.92E+00	4.23E+06
45012.60	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>3/2</sub> )	-0.070	2.13E-01	7.00E+05
45585.06	4s <sup>2</sup> 10f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>3/2</sub> )	0.687	1.22E+00	2.60E+06
45699.64	4s <sup>2</sup> 10f( <sup>2</sup> F <sub>7/2</sub> )	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>5/2</sub> )	0.840	1.15E+00	2.76E+06
45699.66	4s <sup>2</sup> 10f( <sup>2</sup> F <sub>5/2</sub> )	4s <sup>2</sup> 10d( <sup>2</sup> D <sub>5/2</sub> )	-0.461	5.76E-02	1.85E+05
50565.04	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 9s( <sup>2</sup> S <sub>1/2</sub> )	0.605	2.01E+00	2.63E+06
52021.02	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 9s( <sup>2</sup> S <sub>1/2</sub> )	0.292	9.80E-01	2.42E+06
62011.70	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 4f( <sup>2</sup> F <sub>7/2</sub> )	-0.387	5.13E-02	1.19E+05
64796.22	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>3/2</sub> )	-0.266	1.35E-01	2.15E+05
65293.37	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>5/2</sub> )	0.685	8.07E-01	1.89E+06
66997.23	4s <sup>2</sup> 5d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 4f( <sup>2</sup> F <sub>5/2</sub> )	-0.576	4.42E-02	9.87E+04
67206.60	4s <sup>2</sup> 9p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>3/2</sub> )	0.417	6.53E-01	1.93E+06
75204.88	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 10s( <sup>2</sup> S <sub>1/2</sub> )	0.659	2.28E+00	1.35E+06
77387.40	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 10s( <sup>2</sup> S <sub>1/2</sub> )	0.346	1.11E+00	1.24E+06
96260.29	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>1/2</sub> )	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>3/2</sub> )	-0.194	1.60E-01	2.31E+05
96983.90	4s <sup>2</sup> 10p( <sup>2</sup> P <sub>3/2</sub> )	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>5/2</sub> )	0.757	9.53E-01	1.01E+06
99865.28	4s <sup>2</sup> 9d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 8f( <sup>2</sup> F <sub>5/2</sub> )	0.489	5.14E-01	5.15E+05
125274.19	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 5f( <sup>2</sup> F <sub>7/2</sub> )	-0.127	9.33E-02	5.28E+04
130412.27	4s <sup>2</sup> 6d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 5f( <sup>2</sup> F <sub>5/2</sub> )	-0.300	8.35E-02	4.93E+04
187793.78	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 6f( <sup>2</sup> F <sub>7/2</sub> )	0.089	1.53E-01	3.87E+04
194382.72	4s <sup>2</sup> 7d( <sup>2</sup> D <sub>3/2</sub> )	4s <sup>2</sup> 6f( <sup>2</sup> F <sub>5/2</sub> )	-0.081	1.38E-01	3.65E+04
275824.78	4s <sup>2</sup> 8d( <sup>2</sup> D <sub>5/2</sub> )	4s <sup>2</sup> 7f( <sup>2</sup> F <sub>7/2</sub> )	0.231	2.13E-01	2.48E+04

#### 4. Conclusion

It is clear that the present calculations of energy levels and wavelengths show good agreement with the corresponding available both theoretical and experimental data. We have obtained some new unpublished energy levels, wavelengths and transition probabilities

for these ions. These extensive and the more definitive results may be useful in thermonuclear fusion research and astrophysical applications.

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